

## 1-D motion with friction

**Q:** When there is no friction, the flight time for an object thrown directly upward is  $\tau_0 = 2v_0/g$ .

Assume now that there is friction of the form

$$\begin{aligned} \text{(a)} \quad & \mathbf{F} = -k^* \mathbf{v}, \quad \text{or} \\ \text{(b)} \quad & \mathbf{F} = -k^* v^2, \end{aligned}$$

where  $k^*$  is a constant. If the launch speed  $v_0$  is the same w/ and w/o friction, how does the flight time  $\tau$  with friction compare with  $\tau_0$ ?

**(a)** “Linear” friction case

With  $Oy$  oriented upward the equation of time evolution for the speed is

$$\frac{dv}{dt} \equiv \dot{v} = -kv - g, \quad v(t=0) = v_0, \quad (1)$$

where  $k = k^*/m$  ( $m$  is the mass of the object). The solution of (1) is given by

$$v = -\frac{g}{k} + \left(v_0 + \frac{g}{k}\right) \exp^{-kt}. \quad (2)$$

For the  $y$  co-ordinate we obtain

$$y = -\frac{g}{k}t + \frac{1}{k} \left(v_0 + \frac{g}{k}\right) (1 - \exp^{-kt}). \quad (3)$$

For proper mathematical handling let us denote  $\frac{kv_0}{g} = \varepsilon$  and introduce  $t^* = t/\tau_0$  – the non-dimensional time. In terms of these notations (3) becomes

$$y = \frac{2v_0^2}{g} \frac{1}{\varepsilon} \left[ -t + \frac{1}{2} \left(1 + \frac{1}{\varepsilon}\right) (1 - \exp^{-2\varepsilon t}) \right], \quad (4)$$

where we relabeled  $t^*$  back to  $t$  for simplicity.

By Taylor expansion in the limit  $\varepsilon \ll 1$  – the “weak friction” approximation – (4) becomes

$$y \simeq \frac{2v_0^2}{g} (t - t^2 - \varepsilon t^2). \quad (5)$$

We see that in this case the equation  $y = 0$  gives for the total flight time

$$t = \frac{1}{1 + \varepsilon} < 1, \quad (6)$$

which in terms of dimensional time means that if (weak) friction is present, the flight time  $\tau$

is always smaller than the flight time without friction  $\tau_0$ .

An interesting result is obtained if in (4) we take the limit  $\varepsilon \rightarrow \infty$  (strong friction). One observes that in this case  $y \rightarrow 0$  while for the flight time we get  $t \searrow \frac{1}{2}$ . Of course, one may question whether the linear in  $v$  friction is an appropriate approximation in this limit.

By graphical analysis (see Fig. 1) it can be seen that for  $0 < \varepsilon < \infty$  the solution  $t = t(\varepsilon)$  to the equation  $y = 0$  in (4) is a monotonic function of  $\varepsilon$ , with  $t \rightarrow 1$  as  $\varepsilon \rightarrow 0$ , and  $t \rightarrow 1/2$  as  $\varepsilon \rightarrow \infty$ . Hence, we conclude that the (dimensional) flight time obeys

$$\frac{v_0}{g} < \tau \leq \frac{2v_0}{g}, \quad (7)$$

with equality only when there is no friction.

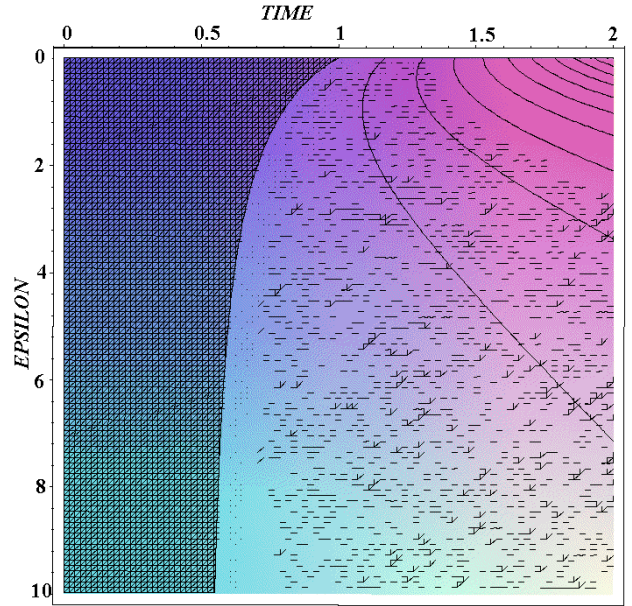


Figure 1: Plot of  $y(t, \varepsilon) = (1/\varepsilon)[-t + (1/2)(1 + 1/\varepsilon)(1 - \exp(-2\varepsilon t))]$  and  $y = 0$  surfaces in  $(\varepsilon, t)$  co-ordinates. For  $\varepsilon \rightarrow 0$  the intersection curve of the two surfaces approaches the line  $t = 1$ , while for large  $\varepsilon$  it goes close to the line  $t = 0.5$ .

**(b)** “Quadratic” friction case

In this case the friction  $F \propto v^2$  and the equations of motion are as follows:

(i) Motion upward (axis  $Oy$  directed upward, origin at the launch point)

$$\dot{v} = -kv^2 - g, \quad v(t=0) = v_0, \quad (8)$$

and the solution is

$$v = \sqrt{\frac{g}{k}} \tan \left( \arctan \sqrt{\frac{k}{g}} v_0 - \sqrt{kg} t \right). \quad (9)$$

The time to reach the highest point of the trajectory is

$$t_u = \frac{1}{\sqrt{kg}} \arctan \sqrt{\frac{k}{g}} v_0 \quad (10)$$

and the maximum height is

$$y_{max} = \frac{1}{2k} \ln \left( 1 + \frac{k}{g} v_0^2 \right) \quad (11)$$

(ii) Motion *downward*: we choose the origin of the reference frame at the highest point ( $Oy$  directed downward). The equation of motion is

$$\dot{v} = -kv^2 + g, \quad v(t=0) = 0, \quad (12)$$

with the solution

$$v = \sqrt{\frac{g}{k}} \frac{\exp(2\sqrt{kg}t) - 1}{\exp(2\sqrt{kg}t) + 1} \quad (13)$$

which in turn gives for the vertical coordinate

$$y = \frac{1}{2k} \left[ 2 \ln(1 + \exp(2\sqrt{kg}t)) - 2\sqrt{kg}t - 2 \ln 2 \right] \quad (14)$$

By equating the above  $y$  with  $y_{max}$  we get the time of descent

$$t_d = \frac{1}{\sqrt{kg}} \ln \sqrt{1 + 2v_0^2 \frac{k}{g} \left( 1 + \sqrt{1 + \frac{g}{kv_0^2}} \right)} \quad (15)$$

We now denote  $\epsilon = v_0 \sqrt{k/g}$  and get the total time of flight  $\tau = t_u + t_d$  as

$$\tau = \frac{v_0}{g} \left\{ \frac{1}{\epsilon} \arctan \epsilon + \frac{1}{2\epsilon} \ln \left[ 1 + 2\epsilon^2 \left( 1 + \frac{\sqrt{1 + \epsilon^2}}{\epsilon} \right) \right] \right\} \quad (16)$$

After a bit of calculus it can be seen that in (16) the multiplier between the curly brackets is bounded to be in the  $(0, 2)$  interval as  $\epsilon$  scans the  $(\infty, 0)$  interval.

Comparison with the time of flight for the frictionless motion,  $\tau_0$ , shows that  $0 < \tau < \tau_0$ .

## Projectile motion with friction

**Q:** It is known that for a given launch speed  $v_0$ , the maximal range is achieved by shooting at  $\alpha_0 = 45^\circ$  (no friction case). If weak friction is present, to get the maximal range for a given  $v_0$  should one aim higher or lower than  $\alpha_0$ ?

When there is no friction the dynamic equations are  $a_x = 0$ ,  $a_y = -g$ , from which we get

$$x = v_0 t \cos \alpha, \quad y = v_0 t \sin \alpha - (g/2)t^2. \quad (17)$$

Eliminating  $t$  between  $x$  and  $y$  expressions we get

$$y = x \tan \alpha - \frac{g}{2v_0^2 \cos^2 \alpha} x^2. \quad (18)$$

For  $y = 0$  we get two solutions for  $x$ , namely the trivial  $x = 0$  and

$$x = \frac{v_0^2 \sin 2\alpha}{g}. \quad (19)$$

For a given  $v_0$  the range  $x_{max}$  is achieved for  $\sin 2\alpha_0 = 1$ , and hence  $\alpha_0 = 45^\circ$ .

Now assume that there is friction of the form  $\mathbf{F}_f = -k^* \mathbf{v}$ . The equations of motion become

$$a_x = -kv_x, \quad a_y = -g - kv_y, \quad (20)$$

with  $k = k^*/m$ . Since  $\dot{v}_x = a_x$ ,  $\dot{v}_y = a_y$ , and the initial conditions are  $v_x(t=0) = v_0 \cos \alpha$ , and  $v_y(t=0) = v_0 \sin \alpha$ , from (20) we get

$$v_x = v_0 \exp^{-kt} \cos \alpha, \quad (21)$$

$$v_y = \left( v_0 \sin \alpha + \frac{g}{k} \right) \exp^{-kt} - \frac{g}{k}. \quad (22)$$

By integrating (21) and (22) one obtains

$$x = \frac{v_0 \cos \alpha}{k} (1 - \exp^{-kt}), \quad (23)$$

$$y = \frac{1}{k} \left( v_0 \sin \alpha + \frac{g}{k} \right) (1 - \exp^{-kt}) - \frac{g}{k} t, \quad (24)$$

which gives the equation of trajectory

$$y = \frac{g}{k^2} \left[ \frac{kx}{v_0 \cos \alpha} \left( 1 + \frac{kv_0 \sin \alpha}{g} \right) + \ln \left( 1 - \frac{kx}{v_0 \cos \alpha} \right) \right] \quad (25)$$

N.B. In the limit  $k \rightarrow 0$ , (25) recovers (18).

We consider the case of a small enough  $k$ , such that  $\eta \equiv (kx/v_0 \cos \alpha) \ll 1$ . We expand the logarithm up to the 3-rd order according to the formula  $\ln(1 - \eta) \simeq -\eta - \eta^2/2 - \eta^3/3$ . We set then  $y = 0$  and obtain that the resulting equation in  $x$  has the nontrivial solution

$$x = \frac{3v_0 \cos \alpha}{4k} \left( \sqrt{1 + \frac{16kv_0}{3g} \sin \alpha} - 1 \right) \quad (26)$$

N.B. In the limit  $k \rightarrow 0$ , (26) recovers (19).

To get the angle  $\alpha$  which provides the extremal value of the range we request that  $\partial x / \partial \alpha = 0$  (simple reasoning convinces us that the extremum is indeed a maximum). Denoting for shortness  $16kv_0/3g = p$ , one gets

$$1 - \sin^2 \alpha = \frac{2}{p} \sin \alpha \left( 1 + p \sin \alpha - \sqrt{1 + p \sin \alpha} \right) \quad (27)$$

Assuming for now the parameter  $p$  to be small, one may expand the square root in (27) and obtain the equation

$$f(z, p) \equiv \frac{p}{4} z^3 + 2z^2 - 1 = 0, \quad (28)$$

where  $\sin \alpha = z$  and we look for solutions around  $z_0 = \sqrt{2}/2 = \sin(\pi/4)$ . One can easily see that the behaviour of  $f(z, p)$  around  $z_0$  is as depicted in Fig.2, whatever  $0 < p \ll 1$  we choose. In particular,  $f(z_0, p) > 0$ , which means that the solution  $z_f$  for (28) obeys  $z_f < z_0$ , which in turn means that  $\alpha_f < \pi/4$  (since  $\sin \alpha$  is a monotonically increasing function for  $\alpha \in (0, \pi/2)$ ). Therefore, in the “weak friction” approximation we have shown that for a given initial speed  $v_0$ , the maximal range is achieved by shooting at an angle  $\alpha_f$  less than  $45^\circ$ .

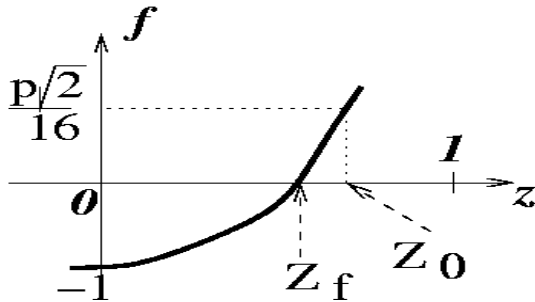


Figure 2: Behaviour of  $f(z, p)$  in the  $[0, 1]$  interval.

*Note 1:* It can be seen that the smallness of  $p$  and  $\eta$  as defined above is related to the smallness of  $k\tau_0$  (where  $\tau_0 = \frac{2v_0 \sin \alpha_0}{g}$  is the time of flight in the frictionless case).

Indeed,  $k\tau_0 \ll 1 \Leftrightarrow p \ll 1$ , since  $2 \sin \alpha_0$  and  $16/3$  are both  $O(1)$ . On the other hand we have

$$\eta = \frac{kx}{2v_0 \cos \alpha} = k\tau_0 \left( \frac{x}{x_{\max}} \right) \frac{\cos \alpha_0}{2 \cos \alpha},$$

where  $x_{\max}$  is given by (19) with  $\alpha_0 = 45^\circ$ . Since we look for solutions with weak friction we expect that  $x \leq x_{\max}$  and  $\frac{\cos \alpha_0}{2 \cos \alpha}$  to be  $O(1)$ . It is true that  $\eta \ll 1 \not\Rightarrow k\tau_0 \ll 1$ , but this is not an issue here.

*Note 2:* One may set  $\sin \alpha = 1$  in (24) and obtain the same results that we got in the first part (1-dimensional motion, case (a)).

As an exercise the reader is asked to try solving the 2-D projectile motion with “quadratic” friction, although the resulting system of ODEs is more complicated (there is no decoupling).